



DEPARTMENT OF FOOD TECHNOLOGY, Heat and Mass Transfer for Food Products

UNIT V - MASS TRANSFER

Topic - Tutorial steady state molecular diffusion

A fluidized coal reactor has been proposed for a new power plant. If operated at 1145 K, the process will be limited by the diffusion of oxygen countercurrent to the carbon dioxide,  $CO_2$ , formed at the particle surface. Assume that the coal is pure solid carbon with a density of  $1.28 \times 10^3 \text{ kg/m}^3$  that the particle is spherical with an initial diameter of  $1.5 \times 10^{-4} \text{ m}$  ( $150 \mu\text{m}$ ). Air (21%  $O_2$  and 79%  $N_2$ ) exists several diameters away from the sphere. Under the conditions of the combustion process, the diffusivity of oxygen in the gas mixture at 1145 K is  $1.3 \times 10^{-4} \text{ cm}^2/\text{s}$ . If a steady-state process is assumed,

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calculate the time necessary to reduce the diameter of the carbon particle to  $5 \times 10^{-5} \text{ m}$  ( $50 \mu\text{m}$ ). The surrounding air serves as an infinite source for  $O_2$  transfer, whereas the oxidation of the carbon at the surface of the particle is the sink for  $O_2$  mass transfer. The reaction at the surface is:





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At the surface of the coal particle, the reaction is so rapid.

Solution:

The pure carbon particle is the source for the CO<sub>2</sub> flux and the sink for O<sub>2</sub> flux. As the coal particle is oxidized, there will be an output of carbon as stipulated by the stoichiometry of the reaction.

Number of moles of oxygen transferred = number of moles of carbon reacted

Number of moles transferred of oxygen = mole flux × area

$$\text{Number of moles transferred of oxygen} = N_{O_2-mix} \times 4\pi r^2$$

$N_{O_2-mix}$  can be obtained by using the general differential equation with the Fick's equation as follows:

By applying the following assumptions on the general differential equation of mass transfer:

$$\nabla \cdot \vec{N}_A + \frac{\partial c_A}{\partial t} - R_A = 0$$

1. Steady state oxygen diffusion
2. One dimensional mass transfer in r direction
3. No homogenous reaction
4. Instantaneous heterogeneous reaction

$$\therefore \nabla \cdot \vec{N}_A = 0$$

For diffusion of oxygen in r-direction

$$\frac{1}{r^2} \frac{d}{dr} (r^2 N_{O_2}) = 0$$



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$$\therefore \frac{d}{dr}(r^2 N_{O_2}) = 0$$

The above equation specifies that  $r^2 N_{O_2}$  is constant over the diffusion path in the r direction, so that

$$r^2 N_{O_2} \Big|_r = R^2 N_{O_2} \Big|_R$$

From Fick's equation:

$$N_{O_2} = -cD_{O_2-mix} \frac{dy_{O_2}}{dr} + y_{O_2}(N_{O_2} + N_{CO_2})$$

But from the stoichiometry of the reaction

$$N_{O_2} = -N_{CO_2}$$

i.e. equimolar counter diffusion

$$\therefore N_{O_2} = -cD_{O_2-mix} \frac{dy_{O_2}}{dr}$$

$$N_{O_2} \int_R^m dr = -cD_{O_2-mix} \int_0^{y_{O_2,\infty}} dy_{O_2}$$

$$N_{O_2} r^2 \int_R^m \frac{dr}{r^2} = -cD_{O_2-mix} \int_0^{y_{O_2,\infty}} dy_{O_2}$$

$$N_{O_2} r^2 \left( \frac{1}{R} \right) = -cD_{O_2-mix} (y_{O_2,\infty} - 0)$$

$$N_{O_2} r^2 = -RcD_{O_2-mix} y_{O_2,\infty}$$

*number of moles of oxygen transferred per unit time =  $N_{O_2} \times 4\pi r^2$*

*number of moles of oxygen transferred per unit time =  $-4\pi R cD_{O_2-mix} y_{O_2,\infty}$*

The negative sign because the transfer of oxygen is in the opposite direction of r

*$\therefore$  number of moles of carbon consumed per unit time =  $4\pi R cD_{O_2-mix} y_{O_2,\infty}$*



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By applying the law of conservation of mass on the carbon:

$$\text{Input} - \text{output} + \text{generation} - \text{consumption} = \text{accumulation (rate of change)}$$

$$- \text{consumption} = \text{accumulation (rate of change)}$$

$$-4\pi R c D_{O_2-\text{mix}} y_{O_2,\infty} = \frac{dN}{dt} = \frac{\rho_c}{M. wt} \frac{dV}{dt}$$

$$V = \frac{4}{3}\pi R^3$$

$$-4\pi R c D_{O_2-\text{mix}} y_{O_2,\infty} = \frac{\rho_c}{M. wt} 4\pi R^2 \frac{dR}{dt}$$

$$dt = - \frac{\rho_c}{M. wt} \frac{R dR}{c D_{O_2-\text{mix}} y_{O_2,\infty}}$$

by integrating the above equation between the limits:

$$\text{at } t = 0 \quad R = R_i = 7.5 \times 10^{-5} \text{ m}$$

$$\text{at } t = t \quad R = R_f = 2.5 \times 10^{-5} \text{ m}$$

$$\int_0^t dt = - \frac{\rho_c}{M. wt} \frac{1}{c D_{O_2-\text{mix}} y_{O_2,\infty}} \int_{R_i}^{R_f} R dR$$

$$t = \frac{\rho_c}{2 M. wt} \frac{(R_i^2 - R_f^2)}{c D_{O_2-\text{mix}} y_{O_2,\infty}}$$

$$c = \frac{P}{RT} = 0.0106 \text{ kmol/m}^3$$

$$y_{O_2,\infty} = 0.21$$

$$\therefore t = 0.92 \text{ s}$$



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**References:**

1. Kothandaraman C.P “Fundamentals of Heat and Mass Transfer” New Age International, New Delhi, 4<sup>th</sup> Edition 2012 (Unit I, II, III, IV, V).
2. Frank P. Incropera and David P. DeWitt, “Fundamentals of Heat and Mass Transfer”, John Wiley and Sons, New Jersey, 6<sup>th</sup> Edition 1998 (Unit I, II, III, IV, V)
3. MIT open courseware – <https://ocw.mit.edu/courses/mechanical-engineering>

Other web sources